

AD-A165 450

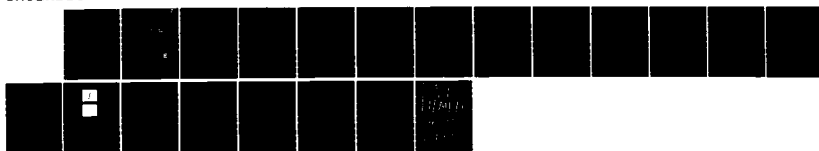
EFFECT OF MAGNETOSTRICTION ON REMANENT MAGNETIZATION  
(U) MASSACHUSETTS INST OF TECH LEXINGTON LINCOLN LAB  
G F DIONNE 05 DEC 85 TR-737 ESD-TR-85-292  
F19628-85-C-0002

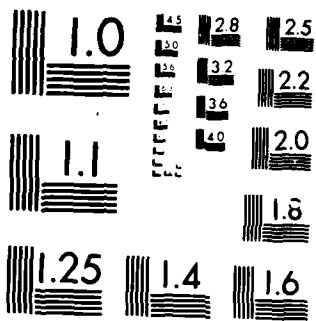
1/1

UNCLASSIFIED

F/G 20/3

NL





MICROCOPY RESOLUTION TEST CHART  
1010 - NATIONAL BUREAU OF STANDARDS-1963-A

AD-A165 450

Technical Report  
737

# Effect of Magnetostriction on Remanent Magnetization

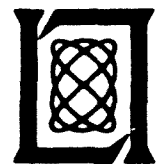
G.F. Dionne

5 December 1985

---

**Lincoln Laboratory**  
MASSACHUSETTS INSTITUTE OF TECHNOLOGY  
*LEXINGTON, MASSACHUSETTS*

---



Prepared for the Department of the Army  
under Electronic Systems Division Contract F19628-85-C-0002.

Approved for public release; distribution unlimited.

The work reported in this document was performed at Lincoln Laboratory, a center for research operated by Massachusetts Institute of Technology. This program is sponsored by the Ballistic Missile Defense Program Office, Department of the Army; it is supported by the Ballistic Missile Defense Advanced Technology Center under Air Force Contract F19628-85-C-0002.

This report may be reproduced to satisfy needs of U.S. Government agencies.

The views and conclusions contained in this document are those of the contractor and should not be interpreted as necessarily representing the official policies, either expressed or implied, of the United States Government.

The ESD Public Affairs Office has reviewed this report, and it is releasable to the National Technical Information Service, where it will be available to the general public, including foreign nationals.

This technical report has been reviewed and is approved for publication.

FOR THE COMMANDER

A handwritten signature in black ink, reading "Thomas J. Alpert". The signature is stylized with a large, sweeping initial 'T' and a long, horizontal stroke at the end.

Thomas J. Alpert, Major, USAF  
Chief, ESD Lincoln Laboratory Project Office

Non-Lincoln Recipients

**PLEASE DO NOT RETURN**

Permission is given to destroy this document  
when it is no longer needed.

MASSACHUSETTS INSTITUTE OF TECHNOLOGY  
LINCOLN LABORATORY

**EFFECT OF MAGNETOSTRICTION  
ON REMANENT MAGNETIZATION**

*G.F. DIONNE*  
*Group 33*

TECHNICAL REPORT 737

5 DECEMBER 1985

*Approved for public release; distribution unlimited.*

LEXINGTON

MASSACHUSETTS

## ABSTRACT

Magnetostriction effects on remanent magnetization are examined in a phenomenological model that is used to design a high magnetization polycrystalline spinel ferrite with excellent square hysteresis loop properties. Isotropic magnetostriction is compensated by substituting  $\text{Mn}^{3+}$  ions for 0.2  $\text{Fe}^{3+}$  ions per formula unit of  $\text{Ni}_{.65}\text{Zn}_{.35}\text{Fe}_2\text{O}_4$  host material. As predicted by theory, the magnetostriction reduction dramatically increases the remanent magnetization and removes most of its external stress sensitivity. The resulting remanent magnetization, which approaches 4000 G, represents an increase of more than a factor of 2 over that of the host composition, with no significant deterioration in other magnetic and dielectric properties. The remanence ratio improvement is in general accord with estimates predicted by the theoretical model.

3

## TABLE OF CONTENTS

Abstract	ii
List of Illustrations	iv
List of Tables	iv
1. INTRODUCTION	1
2. THEORETICAL CONSIDERATIONS	2
A. Phenomenological Model	2
B. Chemical Composition	5
3. EXPERIMENTAL RESULTS	7
4. SUMMARY	11
Acknowledgments	11
References	12

## LIST OF ILLUSTRATIONS

Figure No.		Page
1	Hysteresis Effects of Magnetization and Magnetostriction	2
2	Reduction of Remanent Magnetization $M_r$ by Magnetostrictive Demagnetization	3
3	R Versus $R_1$ for $n = 1, 2$ , and 3	4
4	Comparison of Low Field Hysteresis Loops of $\text{Ni}_{.65}\text{Zn}_{.35}\text{Fe}_2\text{O}_4$ and $\text{Ni}_{.65}\text{Zn}_{.35}\text{Fe}_{1.8}\text{Mn}_{.2}\text{O}_4$	7
5	External Stress Sensitivity of (a) $\text{Ni}_{.65}\text{Zn}_{.35}\text{Fe}_2\text{O}_4$ and (b) $\text{Ni}_{.65}\text{Zn}_{.35}\text{Fe}_{1.8}\text{Mn}_{.2}\text{O}_4$ . Compressive Stress of About $5 \times 10^7 \text{ dyn-cm}^{-2}$ Applied Parallel to the Magnetic Field Normally Increases the Remanent Magnetization in These Materials	8
6	Comparison of Measured Loop of $\text{Ni}_{.65}\text{Zn}_{.35}\text{Fe}_2\text{O}_4$ with Calculated Estimate Based on Equation (4). The Sign of $H_c$ Is Always Chosen to Oppose Domain Wall Motion	9

## LIST OF TABLES

Table No.		Page
I	Magnetostriction Constant Values (300 K)	5
II	Magnetic and Dielectric Data (300 K)	9

# EFFECT OF MAGNETOSTRICTION ON REMANENT MAGNETIZATION

## 1. INTRODUCTION

Polycrystalline ferrite materials with square hysteresis loops can be difficult to obtain for a number of reasons. The demagnetizing effects that determine the magnetization in the remanent state (i.e., zero applied magnetic field) arise from averaged magnetocrystalline anisotropy of randomly oriented grains, closure and reverse domains at pores and grain boundaries, and magnetostriction which can in turn influence both anisotropy and domain wall energies. In this report, the phenomenon of demagnetization from magnetostrictive strains will be examined.

A comprehensive discussion of the effects of magnetostriction on the creation of reverse domains was published by Goodenough.<sup>1</sup> This theory helped to explain the use of external stress in compensating magnetostriction effects to achieve square loops in memory cores. The effect of uniaxial stress on the magnetocrystalline anisotropy was later analyzed by Dionne,<sup>2,3</sup> who drew conclusions similar to Goodenough, but also placed the concept on a more quantitative basis by a demonstration of how magnetostriction compensation through  $Mn^{3+}$  additions could produce stress-insensitive iron garnet compositions. A further result of this work was the discovery that the amount of  $Mn^{3+}$  required for cancellation of external stress effects also produced a maximum remanent magnetization,<sup>4</sup> confirming to some extent the predictions of the Goodenough theory.

In this present work, we shall introduce a simple theoretical concept to explain magnetostrictive demagnetization, and then apply its results to analyze the characteristics of a high magnetization NiZn spinel ferrite with square hysteresis loop properties.

## 2. THEORETICAL CONSIDERATIONS

### A. Phenomenological Model

For isotropic (polycrystalline) materials, magnetostriction phenomena feature hysteresis behavior<sup>5</sup> similar to the magnetization process (see Figure 1). This result is not unexpected because of the cause-and-effect relation between magnetocrystalline anisotropy and lattice stress. As the applied field  $H$  rotates the magnetization  $M$  into a hard direction, the attendant stress produces a magnetostriction strain  $\lambda$  of energy  $(1/2) C\lambda^2$  in the direction of  $H$ , where  $C$  is the Young's Modulus. As a consequence, this magnetoelastic coupling produces a monotonic relation between  $M$  and  $\lambda$  components in the direction of  $H$ . With the magnetic field removed,  $M_r$  and  $\lambda_r$  represent the remanent magnetization and magnetostriction.

Consider as a general assumption that  $M = M_s f(H)$  and  $\lambda = \lambda_s g(H)$ , where the subscript  $s$  refers to the saturation values. If we also assume for convenience that  $g(H) = [f(H)]^n$ , where  $n > 0$ , it follows that

$$\lambda = \lambda_s (M / M_s)^n \quad (1)$$

At remanence, the material is in a state of strain with energy  $(1/2) C\lambda_r^2$ .

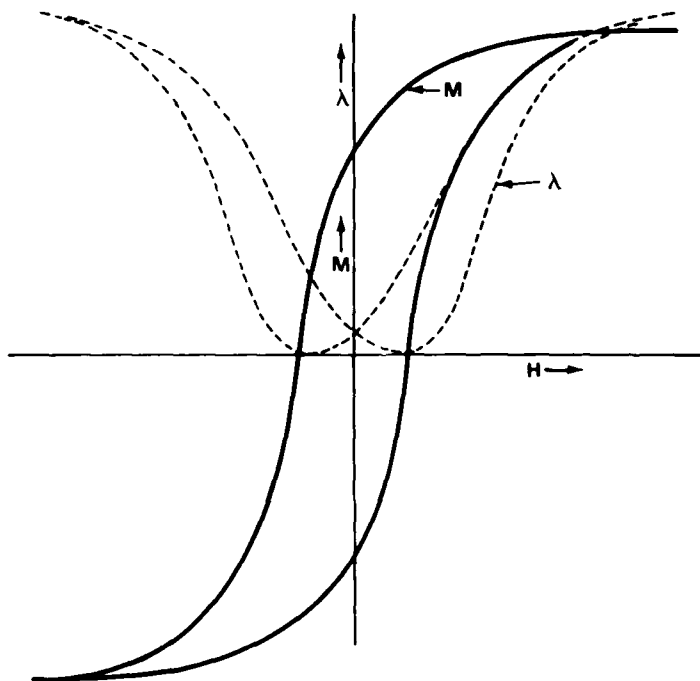


Figure 1. Hysteresis effects of magnetization and magnetostriction.

As depicted in Figure 2, the internal stress causing the strain may be relieved if part of the magnetization changes its direction, thereby reducing  $M_r$  and establishing a new energy equilibrium. If the coercive field  $H_c$  is treated as a bias field in the direction of  $H$ ,\* then it follows that the internal stress must produce its own effective field to overcome the coercive field  $H_c$  and create partial switching or demagnetizing domains. If we express the system energy density as the sum of strain and magnetic contributions,

$$E = (1/2) C \lambda^2 - M H_{\text{eff}} \quad (2)$$

or, with substitution for  $\lambda$  from Equation (1)

$$E = (1/2) C \lambda_s^2 (M/M_s)^{2n} - M H_{\text{eff}} \quad (3)$$

where  $H_{\text{eff}} = H + H_c$ . After minimizing  $E$  with respect to  $M$  (i.e.,  $dE/dM = 0$ ) we find that the equilibrium magnetization is determined by

$$M/M_s = (H_{\text{eff}} M_s / n C \lambda_s^2)^{1/(2n-1)} \quad (4)$$

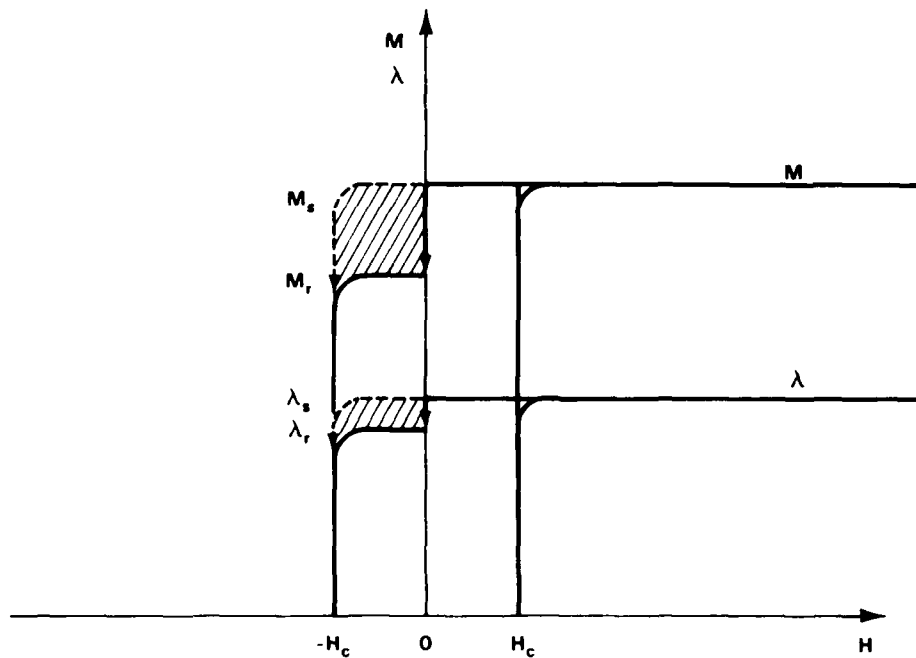


Figure 2. Reduction of remanent magnetization  $M_r$  by magnetostrictive demagnetization.

\* The sign of  $H_c$  in this context would always be in the sense that opposes domain wall motion. Thus, if the applied field were increasing toward saturation,  $H_c$  would be of opposite sign; if  $H$  were becoming smaller, as it approaches remanence in this case,  $H_c$  would reinforce it. This definition is used in the construction of the curves in Figure 6.

For the specific case of  $H = 0$  (i.e., at remanence), Equation (4) is reduced to:

$$R = M_r / M_s = (R_1/n)^{1/(2n-1)} \quad \text{for } 0 \leq R \leq 1 \quad (5)$$

where  $R_1 = H_c M_s / C \lambda_s^2$ . In Figure 3,  $R$  is plotted as a function of  $R_1$  for  $n = 1, 2$ , and  $3$ .

Two comments are appropriate here. First, the direct dependence of  $R$  on  $H_c$  points to a higher degree of magnetostrictive demagnetization where the coercive field is small. Second, the inverse dependence of  $R$  on  $\lambda_s^2$  indicates not only its high sensitivity to magnetostriction, but also its independence of the sign of  $\lambda_s$ . Unlike the external stress effect which can cause  $R$  to increase or decrease according to the relation between the respective signs of  $\lambda_s$  and external stress  $\sigma$  (Reference 3), i.e., whether the applied stress reinforces or opposes the internal stress, the magnetostrictive strain caused by internal stress will always decrease  $R$  in proportion to  $\lambda_s^2$ .

An additional effect of magnetostriction can be a decrease in  $H_c$ . According to Lee,<sup>6</sup> the magnetocrystalline anisotropy  $K_1 = K_0 + \Delta K$ , where  $K_0$  and  $\Delta K$  are the unstrained and magnetostrictive contributions, respectively. For a crystal of cubic symmetry

$$\Delta K = (9/4) [(c_{11} - c_{12}) \lambda_{100}^2 - 2c_{44} \lambda_{111}^2] \quad (6)$$

where  $\lambda_{100}$  and  $\lambda_{111}$  are the respective magnetostriction constants along  $[100]$  and  $[111]$  axes, and  $c_{ij}$  represents the elastic constants. Since the strain energy occurs as a result of stress caused by

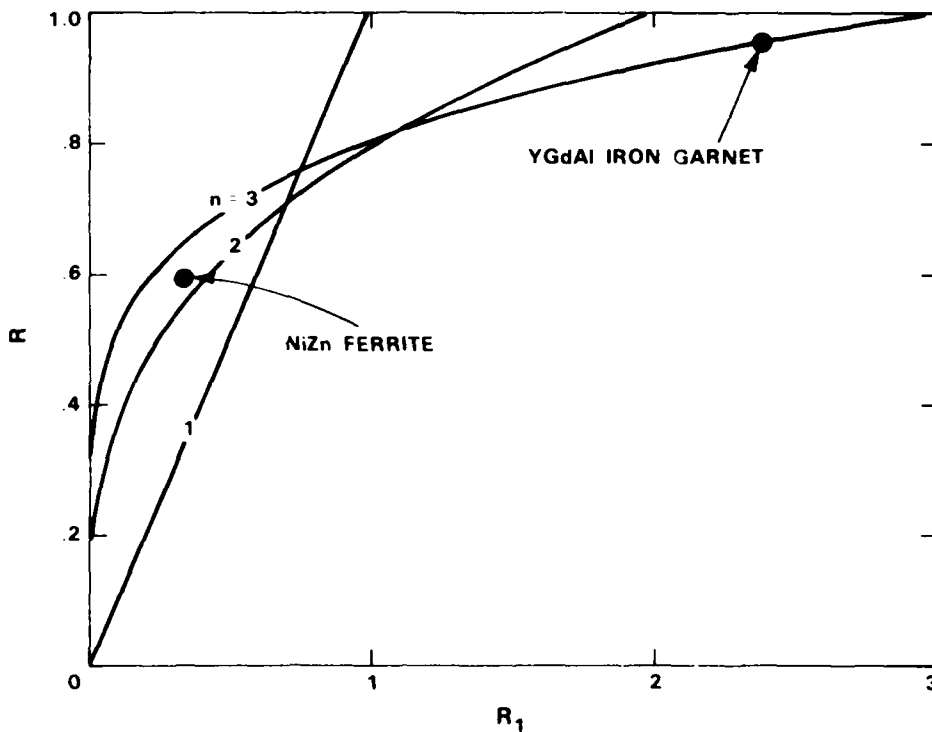


Figure 3.  $R$  versus  $R_1$  for  $n = 1, 2$ , and  $3$ .

anisotropy, it is expected that the net anisotropy would be reduced and that  $K_0$  and  $\Delta K$  would be of opposite sign.

A decrease in the magnitude of  $K_1$  would not only facilitate the demagnetization effect discussed above by lowering domain wall energies to reduce  $H_c$ , but would also raise the initial permeability. Magnetostriction is at least partly responsible for the correlation between low remanent magnetization and high initial permeability.

## B. Chemical Composition

To test the above model with a spinel ferrite, a commercial nickel-zinc ferrite\* closely based on the composition  $\text{Ni}_{0.65}\text{Zn}_{0.35}\text{Fe}_2\text{O}_4$  was chosen as the reference host because of its low remanence ratio and coercive field, and high magnetostriction.

Applying the general relation for the isotropic magnetostriction constant for a cubic lattice,  $\lambda_s = (2/5) \lambda_{100} + (3/5) \lambda_{111}$ , we calculate room temperature  $\lambda_s$  values from the data in Table I for  $\text{NiFe}_2\text{O}_4$  (Reference 7) as  $31 \times 10^{-6}$  and  $\text{MgFe}_2\text{O}_4$  (Reference 8) as  $3 \times 10^{-6}$ . Since the  $\text{Fe}^{3+}$  content is the same for both, we may use the single-ion approximation to estimate the  $\text{Ni}^{2+}$  contribution as  $\lambda_s(\text{Ni}) = \lambda_s(\text{NiFe}_2) - \lambda_s(\text{Fe}_2) = -28 \times 10^{-6}$ . For the  $\text{Ni}_{0.65}\text{Zn}_{0.35}\text{Fe}_2\text{O}_4$  composition,  $\lambda_s = 0.65\lambda_s(\text{Ni}) + \lambda_s(\text{Fe}_2) = -21 \times 10^{-6}$ . Since  $\text{Mn}^{3+}$  ions have been used to compensate  $\lambda_s$  in both  $\text{MgFe}_2\text{O}_4$  (Reference 8) and  $\text{Li}_5\text{Fe}_{1.5}\text{O}_4$  (Reference 9), it is logical that  $\text{Mn}^{3+}$  ions should have similar effects in the NiZn ferrite family.

TABLE I Magnetostriction Constant Values (300 K)				
Composition	$\lambda_{100}$ ( $\times 10^{-6}$ )	$\lambda_{111}$ ( $\times 10^{-6}$ )	$\lambda_s$ ( $\times 10^{-6}$ )	Reference
$\text{NiFe}_2\text{O}_4$	-45.9	21.6	31	7
$\text{MgFe}_2\text{O}_4$	-11.1	+2.3	3	8
$\text{Ni}_{0.65}\text{Zn}_{0.35}\text{Fe}_2\text{O}_4$	-33.7	13.2	-21	estimate
$\text{Y}_3\text{Fe}_5\text{O}_{12}$	-1.3	2.7	2.1	3
$\text{Y}_3\text{Fe}_{4.74}\text{Mn}_{0.26}\text{O}_{12}$	+16.2	+1.1	+7.1	3

\* Catalog No. FI 2-111, Trans-Tech, Inc.

Based on the results of the successful  $\lambda_s$  compensation in  $\text{Y}_3\text{Fe}_5\text{O}_{12}$  (YIG), the single-ion  $\lambda_s$  contribution of octahedral-site  $\text{Mn}^{3+}$  ions as postulated in the local-site distortion model reported earlier<sup>10</sup> is expected to be about  $+36 \times 10^{-6}$  per  $\text{Mn}^{3+}$  ion per formula unit in the garnet lattice. If this quantity is scaled to the spinel lattice where there are 3/8 fewer cations per formula unit, its value increases (by 8/3) to  $+95 \times 10^{-6}$ . Pursuing this reasoning one step further, we find that magnetostriction compensation ( $\lambda_s = 0$ ) should occur with about 0.2  $\text{Mn}^{3+}$  ions per formula unit to balance the  $-21 \times 10^{-6}$  value of the host material. As a consequence, the composition chosen was  $\text{Fe}_{65}^{3+}\text{Zn}_{35}^{2+}[\text{Ni}_{65}^{2+}\text{Fe}_{15}^{3+}\text{Mn}_{25}^{3+}]\text{O}_4$

### 3. EXPERIMENTAL RESULTS

The test specimens were cut from sintered bars of high density prepared by conventional ceramic techniques. In Figure 4 the room temperature hysteresis loops of the NiZn and NiZnMn ferrites prepared under identical conditions are compared to demonstrate the dramatic effect of  $\lambda_s$  compensation by  $\text{Mn}^{3+}$  ion substitutions. The remanent magnetization  $4\pi M_r$  increased by a factor of 2 to approach 4000 G, with only a small increase in coercive field. Verification of the near elimination of magnetostriction was established by the sharp decrease in the sensitivity of  $4\pi M_r$  to a uniaxial external compressive stress (see Figure 5). Values of other parameters are presented in Table II, together with earlier unpublished data on remanence ratio enhancement with  $\text{Mn}^{3+}$  substitution into an YGdAl iron garnet composition.

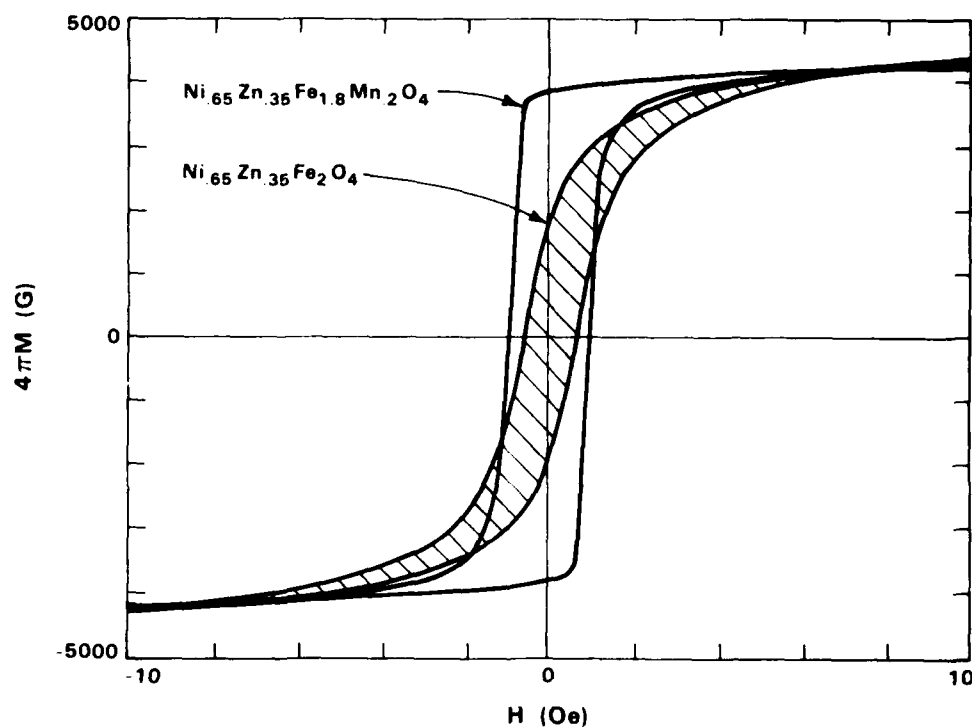
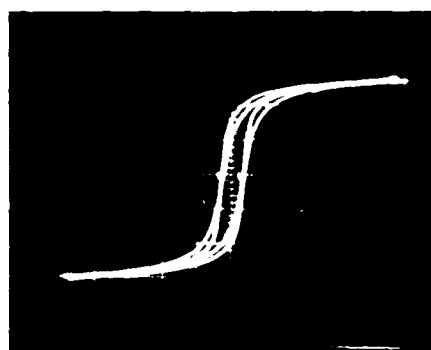
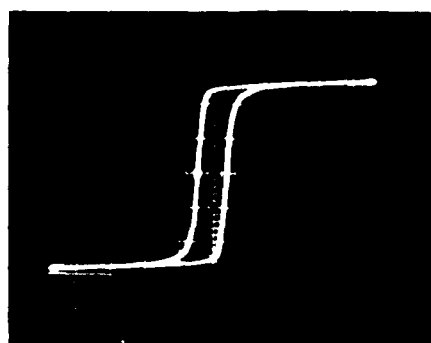


Figure 4. Comparison of low field hysteresis loops of  $\text{Ni}_{65}\text{Zn}_{35}\text{Fe}_2\text{O}_4$  and  $\text{Ni}_{65}\text{Zn}_{35}\text{Fe}_{1.8}\text{Mn}_{0.2}\text{O}_4$ .



(a)



(b)

Figure 5. External stress sensitivity of (a)  $\text{Ni}_{0.65}\text{Zn}_{0.35}\text{Fe}_2\text{O}_4$  and (b)  $\text{Ni}_{0.65}\text{Zn}_{0.35}\text{Fe}_{1.8}\text{Mn}_2\text{O}_4$ . Compressive stress ( $\sim 5 \times 10^7 \text{ dyn-cm}^{-2}$  in this case) applied parallel to the magnetic field normally increases the remanent magnetization in these materials.

If we assume that  $C \approx 30 \times 10^{11} \text{ dyn-cm}^{-2}$  and  $H_c \approx 1 \text{ Oe}$  for both NiZn ferrite ( $M_s = 400 \text{ G}$ ) and the iron garnet composition ( $M_s = 64 \text{ G}$ ) in Table II, and that the respective uncompensated  $\lambda_s$  values are approximately  $-21 \times 10^{-6}$  and  $3 \times 10^{-6}$ , the  $R_1$  value would be 0.36 for the NiZn ferrite and 2.4 for the YGdAl iron garnet. From the curves of Figure 3, the  $R$  decreases from magnetostrictive demagnetization in each case could be explained by a value of  $n$  in the 2 to 3 range.

In Figure 6, Equation (4) is plotted as a function of  $H$  applied for  $R_1 = 0.36$  and  $n = 2.5$  in an attempt to simulate the magnetostrictive effects on the low field hysteresis loop. The discrepancy between the calculated and measured curves shows the influence of anisotropy and microstructural demagnetization which were not taken into account by the simple theoretical model.

TABLE II				
Magnetic and Dielectric Data (300 K)				
Parameter	NiZn Spinel	NiZnMn Spinel	YGdAl Garnet	YGdAlMn Garnet
$4\pi M_s$ (G)	4960	4697	775	747
$4\pi M_r$ (G)	1900	3819	480	508
R	0.38	0.81	0.62	0.68
$\Delta R$	—	+0.43	—	+0.06
$H_c$ (Oe)	0.7	1.0	0.9	1.4
Dielectric Constant	12.38	12.48	14.82	14.91
Dielectric Loss Tangent at 9 GHz	$<10^{-3}$	$<10^{-3}$	$<2 \times 10^{-4}$	$<2 \times 10^{-4}$

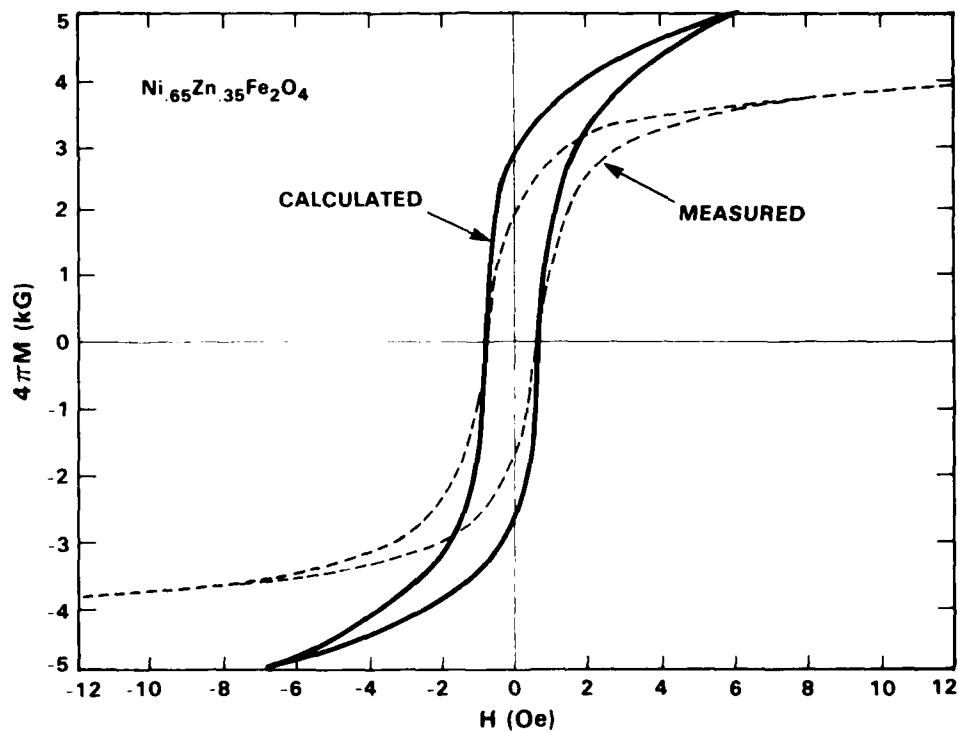


Figure 6. Comparison of measured loop of  $\text{Ni}_{0.65}\text{Zn}_{0.35}\text{Fe}_2\text{O}_4$  with calculated estimate based on Equation (4). The sign of  $H_c$  is always chosen to oppose domain wall motion.

The observed change in  $H_c$  with the substitution of  $Mn^{3+}$  ions is consistent with the prediction of Equation (6). If the increase in  $H_c$  is attributed to the effective elimination of magnetostriction, then  $\Delta K$  for the host composition must be of opposite sign to  $K_1$  and of significant magnitude. To make this computation, we use the  $\lambda_{100}$  and  $\lambda_{111}$  estimates listed in Table I and the elastic constants for  $MgAl_2O_4$  spinel  $c_{11} = 30.0 \times 10^{11}$ ,  $c_{12} = 15.2 \times 10^{11}$ , and  $c_{44} = 15.9 \times 10^{11}$  dyn-cm<sup>-2</sup> (Reference 11). In this manner,  $\Delta K$  is estimated to be greater than  $+10^3$  ergs-cm<sup>-3</sup>, as compared with a typical  $K_1$  value of the order of  $-10^4$  ergs-cm<sup>-3</sup>.

#### 4. SUMMARY

Enhancement of remanent magnetization in spinel and garnet ferrites, particularly those with low coercive fields, may be achieved through reduction of magnetostriction. The phenomenon of stress demagnetization may be interpreted as a decrease in energy by partial switching of the magnetization direction to relieve magnetostrictive strains in the remanent state. Cancellation of the isotropic magnetostriction constant may thus remove the internal stress demagnetization, as well as the sensitivity to external stress. The predictions of this simple theoretical model were verified by the dramatic increase in the remanent magnetization when a designed concentration of  $Mn^{3+}$  ions was used to reduce magnetostriction in a high magnetization NiZn spinel ferrite composition. Complete magnetostriction compensation in this NiZn ferrite family appears to be possible by composition refinements currently in progress.

#### ACKNOWLEDGMENTS

The author is grateful to D.H. Temme and R.W. Sudbury for helpful suggestions, and to R.G. West and D.M. Firor of Trans-Tech, Inc., for preparing the ferrite material according to specifications and for supplying additional data.

## REFERENCES

1. J.B. Goodenough, Phys. Rev. **95**, 917 (1954).
2. G.F. Dionne, IEEE Trans. Mag. **MAG-5**, 596 (1969), DDC AD-703524.
3. ———, IEEE Trans. Mag. **MAG-7**, 715 (1971), DDC AD-737934.
4. G.F. Dionne, P.J. Paul, and R.G. West, J. Appl. Phys. **41**, 1411 (1970).
5. B.A. Wise, "Design of Nickel Magnetostriction Transducers," The International Nickel Company, Inc., 30 September 1955, DDC AD-096417.
6. E.W. Lee, Repts. Prog. Phys. **XVIII**, 184 (1955).
7. A.B. Smith and R.V. Jones, J. Appl. Phys. **37**, 1001 (1966).
8. G.F. Dionne, J. Appl. Phys. **41**, 831 (1970), DDC AD-707583.
9. ———, J. Appl. Phys. **40**, 4486 (1969), DDC AD-703756.
10. ———, J. Appl. Phys. **50**, 4263 (1979), DTIC AD-A0770208-7.
11. D.H. Chung, "Selected Materials for Use in Microsound Circuits and Components. Their Elastic, Piezoelectric, and Dielectric Parameters," Technical Note 1969-29, Lincoln Laboratory, M.I.T. (8 May 1969), DDC AD-692111.

## UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER ESD-TR-85-292	2. GOVT ACCESSION NO AD-A165 450	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) Effect of Magnetostriction on Remanent Magnetization		5. TYPE OF REPORT & PERIOD COVERED Technical Report
		6. PERFORMING ORG. REPORT NUMBER Technical Report 737
7. AUTHOR(s) Gerald E. Dionne		8. CONTRACT OR GRANT NUMBER(s) F19628-85-C-0002
9. PERFORMING ORGANIZATION NAME AND ADDRESS Lincoln Laboratory, M.I.T. P.O. Box 73 Lexington, MA 02173-0073		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS Program Element No. 63304A
11. CONTROLLING OFFICE NAME AND ADDRESS Ballistic Missile Defense Program Office Department of the Army P.O. Box 15280 Arlington, VA 22215		12. REPORT DATE 5 December 1985
		13. NUMBER OF PAGES 17
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) Electronic Systems Division Hanscom AFB, MA 01731		15. SECURITY CLASS. (of this Report) Unclassified
		15a. DECLASSIFICATION DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report)  Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES  None		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number)  remnant magnetization increase      square hysteresis loop NiZn ferrite magnetostriction compensation      high magnetization/low coercivity ferrite stress demagnetization		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number)  Magnetostriction effects on remanent magnetization are examined in a phenomenological model that is used to design a high magnetization polycrystalline spinel ferrite with excellent square hysteresis loop properties. Isotropic magnetostriction is compensated by substituting $Mn^{3+}$ ions for 0.2 $Fe^{3+}$ ions per formula unit of $Ni_{0.65}Zn_{0.35}Fe_2O_4$ host material. As predicted by theory, the magnetostriction reduction dramatically increases the remanent magnetization and removes most of its external stress sensitivity. The resulting remanent magnetization, which approaches 4000 G, represents an increase of more than a factor of 2 over that of the host composition, with no significant deterioration in other magnetic and dielectric properties. The remanence ratio improvement is in general accord with estimates predicted by the theoretical model.		

END  
FILMED

4-86

DTIC